SECTION III

RADIO-FREQUENCY AMPLIFIER UNIT CRV-50096

TECHNICAL SUMMARY

ELECTRICAL CHARACTERISTICS

Dimensions-

Tuning Range
Number of Bands
Band Coverage 3 to 6 mc, 6 to 12 mc, and 12 to 24 mc
Antenna Matching Impedance
Overall R-F Gain (Approximate)

3 to 6-MC Band	6 to 12-MC Band	12 to 24-MC Band
1,800- 4,700 at 3 mc	1,250-2,300 at 6 mc	3,300- 5,600 at 12 mc
4,100-11,000 at 4.5 mc	3,000-5,100 at 9 mc	5,000-11,000 at 18 mc
5,000-17,000 at 6 mc	3,300-5,400 at 12 mc	3,500- 8,000 at 24 mc
Conversion Gain (average) TUBE COMPLEMENT—		1 to 2
R-F Amplifiers		
Detector		3 RCA-78
MECHANICAL SPECIFICATIO	DNS—	

Panel Size	. 19 inches (width) by $27^{31}/_{32}$ inches (height)
Unit Depth	
Weight (net)	

DESCRIPTION

The radio-frequency amplifier unit has been designed especially for use with the space diversity receiving system. Its purpose is to select and amplify the desired signal and also to convert that signal through heterodyne action to a suitable intermediate frequency. The amplifier stages may be operated either with fixed gain or with automatic gain control (AGC). In the latter case, such control is obtained from one of the associated units comprising the equipment. An outstanding feature of this unit is the isolation of the heterodyne oscillator from the remainder of the circuit, insuring absence of crosstalk between receivers even in large communication stations.

Three separate and complete radio-frequency chains are contained in this unit. Each chain covers one frequency band and consists of an input coupling coil, three stages of tuned r-f amplification, a heterodyne oscillator and a heterodyne detector. Transfer from one band to another is accomplished by means of a threeposition switch that supplies filament voltage to only those tubes in the chain selected. This arrangement provides sufficient flexibility, maximum ease of operation and elimination of troubles generally experienced with plug-in coils. Another advantage is that there are no switch contacts required in the low-loss r-f tuned circuits. The resulting reliability of performance and simplicity of design are well worthwhile, particularly in equipment intended for handling important services.

The use of three r-f bands for covering the total frequency range has several advantages. Since each band covers only a two-to-one frequency range, the input coupling coils are reasonably uniform with respect to noise equivalent and transmission-line loading. The three band ranges correspond approximately to the ranges of frequencies employed during the day time, evening and night hours, respectively. Thus it is possible to pretune the r-f circuit from calibration cards before changing from a day signal to





a night signal, the actual changeover then consisting of only turning the range switch, shifting the input connection and touching-up the tuning adjustments.

Each of the input coupling coils is adjustable to eliminate overloading on very strong signals, such adjustment being provided by the three small knobs on the front of the unit near the top. An electrostatic shield is interposed between each coil and its corresponding tuned circuit to prevent capacitive coupling. Proper performance of the horizontal rhombic and "fishbone" antennas depends upon responsiveness of the entire system to only horizontal polarized waves. This means that the system must be symmetrical with respect to ground and that the output shall be taken only from wire to wire of the transmission line and not from line to ground. Such a condition can be realized only when the coupling between the antenna system and the first tuned circuit is purely inductive. Capacitive coupling would impair the directive characteristics of the antenna system.

All of the r-f circuits are individually tuned to insure maximum selectivity and simplify maintenance. The first tuned circuit of each band is designed to give the lowest possible noise equivalent throughout its frequency range. On the 3to 6-mc and 6- to 12-mc bands, additional damping is provided in the second, third and fourth tuned circuits to keep the variation of gain with respect to frequency within reasonable limits and yet maintain the required selectivity. The fourth tuning inductors are tapped at points to obtain the desired value of overall gain and minimum interaction between the detector grid and heterodyne oscillator circuits. The tracking characteristics of a typical receiver are shown in Figure 1.

Automatic gain control (AGC), is normally employed on all r-f stages. In addition to maintaining constant output from the equipment, this feature serves to keep the signal level at the heterodyne detector reasonably low. Transfer from AGC to fixed bias, or the reverse, is afforded by means of the small toggle switch on the front panel. Manual gain control is available at all times by means of a potentiometer for adjustment of the screen-grid voltage supplied to the amplifier tubes. As noted above, separate tubes are employed for the heterodyne detector and oscillator stages. The screen-grid and bias voltages and the suppressor grid voltage of the detector tube are adjusted to give an essentially linear modulation action. This means that distortion and harmonic generation in the detector stage will be at a minimum. Spurious responses of the receiver as a whole, therefore, will be minimized; also, such frequencies differing from that of the desired signal by submultiples of the output (first intermediate) frequency. The detector output system is designed to work into the tuned input circuit of the associated i-f amplifier unit which is described in Section IV.

To prevent bothersome frequency drift of the heterodyne oscillators when operation is switched from one band to another, the filaments of all three oscillator tubes are kept heated at all times. However, plate voltage is applied only to that tube which is in use, thus eliminating any possibility of spurious beat notes from the other two. In contrast, only the filament circuits of the r-f amplifier tubes are switched when changing frequency bands. Power supply circuits and lowfrequency filtering are common to the three r-f bands with the exception of the oscillators.

Special shielding of the oscillator tank circuit, oscillator tube and associated elements insures freedom from troublesome radiation into the input coupling coils, antenna transmission lines and other receivers. The importance of adequate shielding is apparent when it is considered that approximately ten volts of oscillator signal is applied to the detector tube and that the receiver will operate on input signals of one microvolt or less. There are the three small knobs located on the front of the unit near the bottom to control the oscillator vernier tuning capacitors. The oscillator tubes are located inside the individual rectangular shields (see Figure 3) which are readily detachable upon removing the knobs.

To enable rapid tuning, there is provided on the front panel unit a card file for calibration and signal logging. Ready availability of accurate and complete tuning calibrations will be found to save much time in locating and identifying signals. The card file is divided into three groups, each group corresponding to one of the three frequency bands and distinguished by a separate color. An indicator card listing frequencies throughout the particular band is placed at the top of a group of ten signal calibration cards of the same color. The five spaces in each vertical row (on these indicator cards) correspond to the five tuning dials in any one chain of the unit. Dial settings for nominal frequencies are entered during factory test of the equipment.

The signal calibration cards, will each accommodate complete tuning calibration for three signals, one in each of the three vertical columns. The upper five spaces correspond to the dials of any one chain in the unit and dial settings are entered in them. The three spaces at the bottom of each column may be used in various ways.' Usually the space just below the double line is used for entering the designation of the best antenna for that signal, while the second and bottom spaces are employed to designate the call letters and the frequency of the signal. Entering of frequency on the bottom space is advantageous in that it permits arrangement of the calibrations according to frequency. Calibrations for even hundreds of kilocycles may then be inserted between the calibrations for specific signals. These will often be found to be very useful when hunting for new signals or ones not previously used.

OPERATION

Operation of the r-f amplifier unit is covered in sufficient detail under the operation of the system and reference should be made to Section I for procedure. In general, tuning consists of adjusting the unit for operation within the proper frequency band and setting the individual dials for the band involved.

The range switch is located at the left just above the plate milliammeter (see Figure 2) and the three positions are clearly identified by nameplates which indicate the band frequency limits. Corresponding nameplates are provided on the main door of the unit below the respective vertical rows of dials. In each row from top to bottom, the dials serve to control the first, second and third r-f amplifier stages, the heterodyne detector and the oscillator. Input coupling is controlled by the small knobs just below the uppermost dials while vernier tuning of the oscillator is accomplished by the small knobs at the bottom. Choice of AGC or fixed gain is afforded by the toggle switch just beneath the plate milliammeter. The knob slightly to the right of this switch enables manual control of gain in either condition of operation. Recommendations for proper use of the AGC system are included within Section I.

In tuning, the total plate current of the three r-f amplifier stages may be observed on the milliammeter. Jacks are available at the bottom of the panel for determining the individual plate currents of the detector and oscillator circuits.

To facilitate retuning operations, the dial settings for each station should be logged in the card index file. Settings for nominal frequencies are shown on the indicator card preceding each group of signal calibration cards.

SERVICE

In the event of failure within the r-f amplifier unit, reference should be made initially to the portion of Section I dealing with "Maintenance." The proper procedure for locating the defective unit is outlined therein and this section therefore will be limited to specific information for replacement and repair of such parts.

RANGE SWITCH

To replace the range switch, first remove the knob by pulling it forward and turning it counterclockwise until it is loose. The switch itself is then, removed by simply unscrewing the two rear screws which hold it in place on the mounting spacers. Do not attempt to loosen the screws on the front of the unit. If wires must be unsoldered, a fairly large and very hot soldering iron should be used so as to avoid undue heating of the contact arm. All wires should be tagged before removal, to facilitate reconnection when replacement is made.

TUNED CIRCUITS

All design data necessary for rewinding the coil of any tuned circuit assembly are shown in the accompanying table and parts list. Any assembly may be withdrawn simply by removing four screws at the front and detaching the wires which pass through to the rear of the chassis. Care must be taken not to disturb appreciably the arrangement of these wires in removing the assembly from the chassis. This precaution is especially important in the case of the red (plate) leads in the 12- to 24-megacycle assemblies. In no case should this wire be cabled up with the plate supply and bias wire since the tuning calibration at the high-frequency end of the range would be seriously affected. It is possible that the upper limit of the tuning range may be reduced by such practice from somewhat over 24 megacycles to perhaps 22 megacycles, or even lower. The screws which secure the shield cans to the chassis must be kept well tightened to avoid instability or oscillation in the r-f stages.

TUNED CIRCUIT DESIGN DATA

Band		Coil Data	Antenna Coupling	1st RF	2nd RF	3rd RF	Detector	Oscil- lator
3 to 6 MC		Wire Size (AWG No.) Turns per inch Total Turns Bias or ±125 Grid & Plate Damping Ohms Stator of Condenser Grid Rotor ±125 Supply Detector G-3 Plate Stator	36 DSC 20 	28 40 40 20 40 	28 40 40 0 18 100000 40 	28 40 40 0 18 100000 40 	28 40 40 0 18 100000 40 	$ \begin{array}{c} 28 \\ 40 \\ 38 \\ \\ \\ 0 \\ 9 \\ 12^{1/2} \\ 38 \\ \end{array} $
6 to 12 MC		Wire Size (AWG No.) Furns per inch Fotal Turns Bias or ±125 Grid & Plate Damping Ohms Stator of Condenser Grid Rotor ±125 Supply Detector G-3 Plate Stator	36 DSC 10 	22 20 18 0 12 18 	22 20 18 0 9 100000 18 	22 20 18 0 9 100000 18 	22 20 18 0 9 100000 18 	$ \begin{array}{c} 22\\ 20\\ 18\\\\\\ 0\\ 5^{1/2}\\ 7\\ 18\end{array} $
12 to 24 MC	Т	Wire Size (AWG No.) Furns per inch Total Turns Bias or ±125 Grid & Plate Damping Ohms Stator of Condenser Grid Rotor ±125 Supply Detector G-3 Plate Stator	36 DSC 6 — — —	16 10 8 0 8 	16 10 8 0 6 	16 10 8 0 6 	16 10 8 0 6 	$ \begin{array}{c} 16\\ 10\\ 8\\\\\\ 0\\ 2^{1/2}\\ 3^{1/2}\\ 8\end{array} $



Figure 2—Type CRV-50096 Radio-Frequency Amplifier Unit (Front View, Tube Access Door Closed)







Figure 4—Type CRV-50096 Radio-Frequency Amplifier Unit (Rear View, Cover Removed)



Figure 5—Typical Circuit Assembly (First Stage, 3 to 6 MC Band)



Figure 6—Typical Circuit Assembly (Heterodyne Oscillator, 12 to 24 MC Band)







Figure 7—Type CRV-50096 Radio-Frequency Amplifier Unit (Schematic, T-601760—Sub. 5)





